

## Simulation of Irreversible Electro-oxidation on a Partially Blocked Electrode

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### Abstract

An irreversible electrode reaction influenced by the reversible potential dependent inhibition is theoretically analysed. The consequence of reactivation of the electrode surface is the continuation of electro-oxidation and the appearance of the second anodic peak in cyclic voltammetry. An indicator of the change of the electrode kinetics caused by the inhibitor is proposed.

**Keywords:** electrode reactivation, inhibition, partially blocked electrode, simulation.

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### Introduction

Partially blocked electrodes and arrays of microelectrodes may operate under similar diffusion conditions. The mass transport towards an array of microelectrodes on the stationary platform depends on the geometry of electrodes and the distance between them [1 - 5]. The material lying above the insulating part of the platform is diffusing towards the edge of the microelectrode, and thus contributes to the flux. Hence, the diffusion layers of individual electrodes overlap, and the response of the array changes from the sum of responses of the microelectrodes to the response of the planar macroelectrode [2, 6-8]. The arrays of microelectrodes are suitable for use in highly resistive media [9], and for the kinetic measurements using high scan rates [10-11]. Furthermore, they are employed in sensors [5] and in electrosynthesis [12]. Also, they may appear as electrodes modified with catalytically reactive microdroplets of liquid which is not miscible with water [13-14]. Particularly, the electrodes that are inactivated by the adsorption of the inhibitor of a certain electrode reaction are interesting [15 - 17]. To the first approximation, a partially blocked electrode can be considered as an array of inert disks on an electroactive surface [18-19]. A special case of blocked electrodes appears in the electro-oxidation of methanol [20 - 30] and ethanol [31 - 35]. These irreversible electrode reactions are hindered by the adsorption of carbon monoxide [21, 30]. In cyclic voltammetry,

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the inhibitor is adsorbed in the anodic branch and desorbed in the cathodic one. So, the electrode is firstly inactivated and then reactivated. The consequence is an anomalous cyclic voltammogram consisting of anodic peaks in both branches. In this short communication, the simplest model of the influence of partial and complete deactivation and reactivation of the electrode surface in staircase cyclic voltammetry of an irreversible electrode reaction is developed. The purpose of the work is to investigate the influence of the electrode kinetics on the second anodic peak current.

### Model

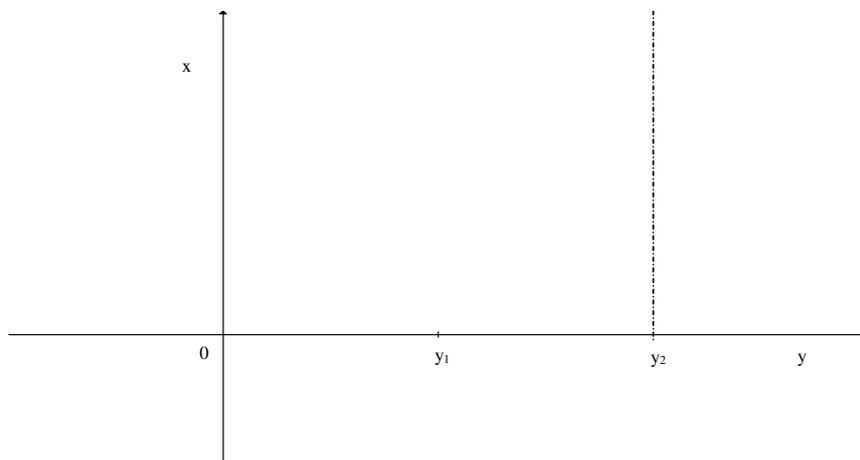
A totally irreversible electro-oxidation of the dissolved reactant giving a dissolved product is considered:



It is imagined that the inactivation and reactivation of the electrode surface are caused by unknown processes that depend on the electrode potential. The ratio of active area and total geometric area of the electrode surface may be changed from one to zero:

$$0 \leq S/S_{tot} \leq 1 \quad (2)$$

For the stationary, planar diffusion, the simplest model is based on the assumption that the electrode surface is covered by equally wide strips of the inhibitor that are separated by equally wide strips of the active area. The edges of the electrode are neglected. The motive that is repeated starts at the middle of the inhibitor strip and finishes at the middle of the active strip. It is shown in Scheme 1.



**Scheme 1.** Diffusion field.

For the purpose of simulation, the motive is divided in twenty increments. The width of the inhibitor can be changed from zero to 20. It is assumed that the inhibitor prevents the transfer of electrons from the reactant to the electrode. Under these conditions, the reaction (1) can be described by the following differential equation and boundary conditions:

$$\partial c_A / \partial t = D(\partial^2 c_A / \partial x^2 + \partial^2 c_A / \partial y^2) \quad (3)$$

$$t = 0, \quad x \geq 0, \quad 0 \leq y \leq y_2: \quad c_A = c_A^* \quad (4)$$

$$t > 0, \quad x \rightarrow \infty, \quad 0 \leq y < y_2: \quad c_A \rightarrow c_A^* \quad (5)$$

$$x = 0, 0 \leq y \leq y_1: \quad \partial c_A / \partial x = 0 \quad (6)$$

$$x = 0, y_1 < y \leq y_2: \quad D \partial c_A / \partial x = I / FS \quad (7)$$

$$x \geq 0, y = 0: \quad \partial c_A / \partial y = 0 \quad (8)$$

$$x \geq 0, y = y_2: \quad \partial c_A / \partial y = 0 \quad (9)$$

$$I / FS = k_s \exp((1 - \alpha)F(E - E^0) / RT) c_{A,x=0} \quad (10)$$

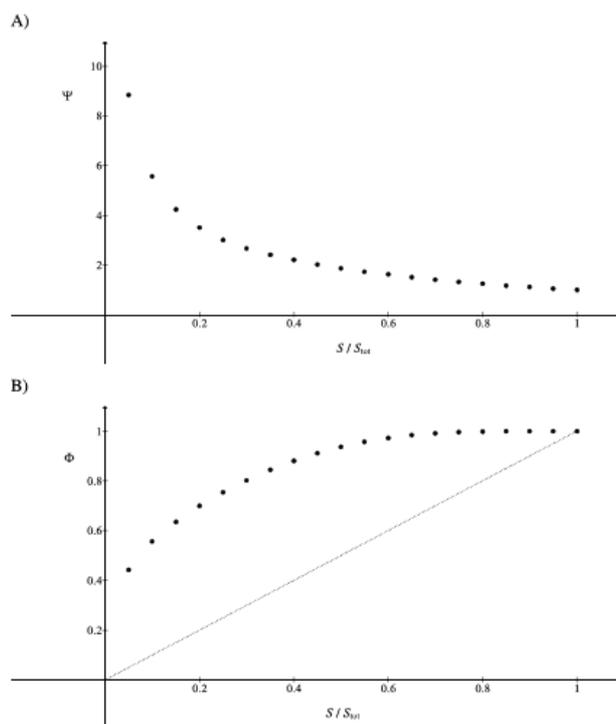
The meanings of the symbols are listed in Table 1. Equation (3) was solved by the digital simulation method [36]. In chronoamperometry, the dimensionless current density,  $\Psi = I(FSc_A^*)^{-1}(\pi t/D)^{1/2}$ , and the average dimensionless current density,  $\Phi = I(FS_{tot}c_A^*)^{-1}(\pi t/D)^{1/2}$ , are calculated as functions of the active area of the electrode surface. The current depends on the dimensionless rate constant  $\lambda = k_s(\pi t/D)^{1/2}$ . In cyclic voltammetry, the average dimensionless current density is defined as  $\Phi = I(FS_{tot}c_A^*)^{-1}(RT/FDv)^{1/2}$ , and the dimensionless rate constant is  $\kappa = k_s(RT/FDv)^{1/2}$ .

**Table 1.** Meaning of symbols.

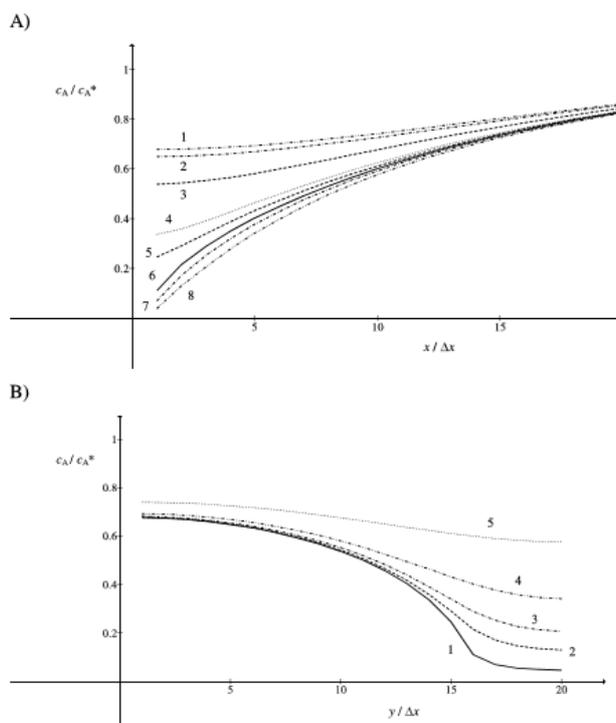
$\alpha$	Transfer coefficient of reaction (1)
$c_A$	Concentration of species A
$c_A^*$	Concentration of species A in the bulk of solution
$D$	Diffusion coefficient
$E$	Electrode potential
$E^0$	Standard potential of the electrode reaction (1)
$\Delta E$	Potential step in staircase cyclic voltammetry
$F$	Faraday constant
$I$	Current
$k_s$	Rate constant of electrode reaction (1)
$R$	Gas constant
$S$	Active area of electrode surface
$S_{tot}$	Total geometric area of electrode surface
$T$	Temperature
$t$	Time
$\tau$	Step duration in staircase cyclic voltammetry
$v$	Scan rate

## Results and discussion

The relationship between the dimensionless current density and the relative area of the active electrode surface is shown in Fig. 1A. The corresponding average current density is shown in Fig. 1B. The density decreases with the increasing active area and tends to be 1 for  $S = S_{tot}$ . As consequence, the average density is bigger than 0.99, if  $S/S_{tot} \geq 0.7$ . This means that the influence of the inhibitor is negligible if it covers less than 30% of the geometric area of the electrode surface. Moreover, on a heavily blocked surface, on which only 5% of the geometric area remains active, the current density increases to 8.83, and the average density decreases only to 0.44, comparing to 0.05 that is expected from the linear relationship between  $\Phi$  and  $S$ .

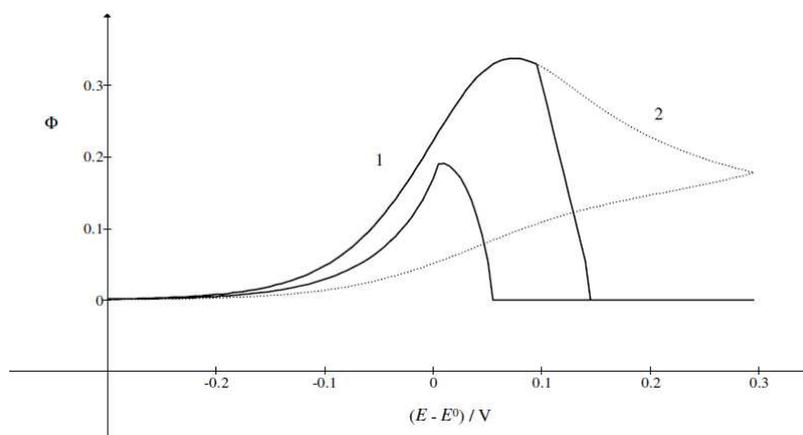


**Figure 1.** Chronoamperometry of an irreversible electro-oxidation reaction (1) on a partially inactive electrode surface. Dependence of dimensionless current density (A) and average current density (B) on an active surface area.  $E - E^0 = 0.3$  V,  $\lambda = 1.25$ ,  $\alpha = 0.5$ ,  $\Delta t = t/1000$  and  $D\Delta t/\Delta x^2 = 0.2$ . A dotted straight line in (B) is the average current density expected for  $\Psi = 1$ .



**Figure 2.** Concentration profiles (A) perpendicular to, and (B) parallel with the electrode surface. (A)  $y/\Delta x = 1$  (1), 5 (2), 10 (3), 14 (4), 15 (5), 16 (6), 17 (7) and 20 (8). (B)  $x/\Delta x = 1$  (1), 2 (2), 3 (3), 5 (4) and 10 (5).  $S/S_{tot} = 0.25$  and all other data are as in Fig. 1.

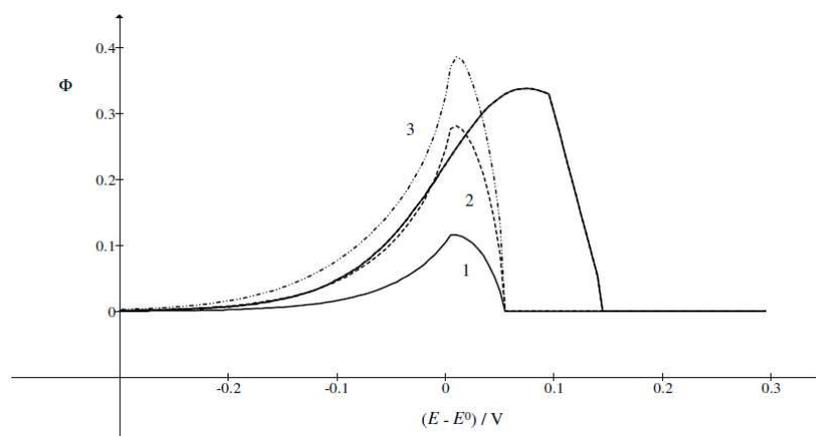
These phenomena are explained in Fig. 2 that shows the concentration profiles at the potential at which the electrode reaction (1) is diffusion controlled. The profiles are calculated for  $S/S_{tot} = 0.25$ . This means that  $y_1/\Delta x = 15$ . Firstly, one can notice that the diffusion layer extends over the blocked surface and that the concentration gradient is the highest on the edge of the active area ( $y/\Delta x = 16$ ) and decreases towards the middle of the active area ( $y/\Delta x = 20$ ). So, the real current density is not uniform over the active area. Looking at Fig. 1, it can be seen that  $\Psi = 3.02$  and  $\Phi = 0.75$  for  $S/S_{tot} = 0.25$ . At the edge of the block ( $y/\Delta x = 15$ ), a strong lateral flux decreases with the increasing distance from the electrode surface. This flux tends to zero at the middle of the block ( $y = 0$ ). These results show that, on a partially blocked electrode, there is no linear relationship between the average current density and the active surface area, and that the influence of the inhibitor cannot be neglected if it covers more than 50% of the geometric surface area.



**Figure 3.** Staircase cyclic voltammograms of the reaction (1) in the presence (1) and the absence (2) of deactivation and reactivation of the electrode surface;  $\kappa = 0.36$ ,  $\Delta E = 5$  mV,  $\Delta t = \tau/50$ ,  $\tau = \Delta E/v$  and all other data are as in Fig. 1.

Fig. 3 shows cyclic voltammograms of the reaction (1). If there is no inactivation of the electrode surface (curve 2), the dimensionless peak current and peak potential are  $\Phi_p = 0.338$  and  $E_p - E^0 = 0.075$  V, respectively. Under the influence of deactivation and reactivation of the electrode surface (curve 1), another anodic peak appears in the reverse, cathodic branch of the voltammogram. Its peak current and potential are  $\Phi_{p,2} = 0.191$  and  $E_{p,2} - E^0 = 0.010$  V. This response was calculated under the assumption that, in the anodic branch, the active area is equal to the geometric area ( $S = S_{tot}$ ) if  $-0.3 \leq (E - E^0)/V < 0.1$ , and that it decreases linearly with the electrode potential between 0.1 V and 0.145 V ( $S/S_{tot} = -20(E - E^0) + 2.9$ ). At the higher potentials, the electrode surface is totally blocked ( $S = 0$ ). In the cathodic branch, the surface remains totally blocked between 0.3 V and 0.055 V, and then the relative active area increases linearly with the potential from 0.055 V to 0.005 V vs.  $E^0$  ( $S/S_{tot} = -20(E - E^0) + 1.1$ ). At lower potentials, the electrode surface

is fully active. In the anodic branch, the voltammogram is not influenced by the inhibitor at potentials lower than 0.1 V vs.  $E^0$  ( $\Phi_{p,1} = 0.338$  and  $E_{p,1} - E^0 = 0.075$  V), but then the current quickly decreases to zero because of the electrode inactivation. In the reverse branch, the current reappears as the consequence of reactivation of the electrode surface. Once the current is diminished to zero, the reactant concentration at the electrode surface increases until the electrode is reactivated. For this reason, the second anodic peak current is higher than the current at the second peak potential, in the absence of deactivation [37]. However, the second peak current is smaller than the current of the anodic branch at the same potential ( $\vec{\Phi}_{E=E_{p,2}}$ ). This is because the initial conditions are not re-established during the electrode deactivation.



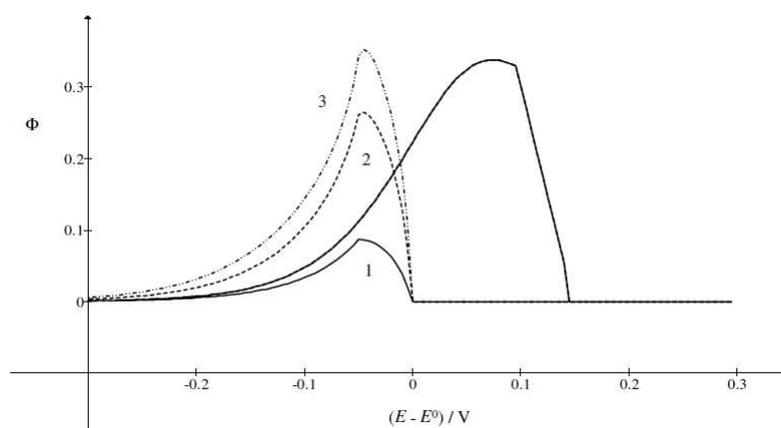
**Figure 4.** Influence of the dimensionless rate constant on the reactivated electrode surface on cyclic voltammograms of the reaction (1).  $\kappa_1 = 0.36$ ,  $\kappa_2 = 0.18$  (1), 0.72 (2) and 1.8 (3). All other data are as in Fig. 3.

In many experiments, it was observed that the second peak current is not much lower than the first peak current. This can be explained by the change of kinetics of the electrode reaction after the reactivation of the electrode surface. Possible examples are shown in Fig. 4. These voltammograms were calculated by assuming that there are two kinetic parameters:  $\kappa_1$ , that applies to the anodic branch and  $\kappa_2$ , applying to the cathodic branch. We are proposing the ratio of the second peak current to the current at the same potential in the anodic branch as the characteristic function of the ratio of  $\kappa_2$  and  $\kappa_1$  kinetic parameters. The voltammogram 1 in Fig. 3 was calculated for  $\kappa_2 = \kappa_1$  and the characteristic ratio is  $\Phi_{p,2}/\vec{\Phi}_{E=E_{p,2}} = 0.77$ . In Fig. 4, the values of this ratio are:  $\Phi_{p,2}/\vec{\Phi}_{E=E_{p,2}} = 0.49, 1.13$  and  $1.56$  for  $\kappa_2/\kappa_1 = 0.5, 2$  and  $5$ , respectively. These two ratios are connected by the following linear relationship:  $\Phi_{p,2}/\vec{\Phi}_{E=E_{p,2}} = 1.13 \log(\kappa_2/\kappa_1) + 0.77$ . The slope of this straight line depends on the difference between the potentials of the first and the second peak, but the intercept is independent of this difference. This is shown in Fig. 5. The voltammograms that are reported in this figure were calculated for the relationship  $S/S_{tot} = -20(E - E^0)$ . This means that the electrode is reactivated between 0 V and -0.050 V vs.  $E^0$ . The potentials of the first and the second peak are 0.075 V and -0.050 V vs.  $E^0$ , respectively,

and the difference between them is 125 mV. The characteristic ratios of the curves in Fig. 5 are as follows:  $\Phi_{p,2}/\vec{\Phi}_{E=E_{p,2}} = 0.77, 2.19$  and  $2.92$  for  $\kappa_2/\kappa_1 = 1, 5$  and  $10$ , respectively. They satisfy the relationship:  $\Phi_{p,2}/\vec{\Phi}_{E=E_{p,2}} = 2.02 \log(\kappa_2/\kappa_1) + 0.77$ . Similar calculations were performed by using several values of the difference  $E_{p,1} - E_{p,2}$ , and the following relationship was found:

$$\Phi_{p,2}/\vec{\Phi}_{E=E_{p,2}} = [12.9 (E_{p,1} - E_{p,2}) + 0.44] \log(\kappa_2/\kappa_1) + 0.77 \quad (11)$$

Eq. (11) applies to  $0.010 < (E_{p,1} - E_{p,2})/V < 0.180$  and  $-0.5 < \log(\kappa_2/\kappa_1) < 1.2$ .



**Figure 5.** Influence of the dimensionless rate constant on the reactivated electrode surface on cyclic voltammograms of the reaction (1).  $\kappa_1 = 0.36$ ,  $\kappa_2 = 0.36$  (1), 1.8 (2) and 3.6 (3). All other data are as in Fig. 3.

In the electro-oxidation of methanol on a platinum electrode, the difference  $E_{p,1} - E_{p,2} = 0.150$  V and the ratio  $I_{p,2}/\vec{I}_{E=E_{p,2}} = 3$  were observed [20]. Using the theoretical relationship between these variables, the ratio  $\kappa_2/\kappa_1 = 8.7$  can be calculated. Also, in the electro-oxidation of ethanol catalysed by palladium, the cyclic voltammogram is characterised by  $E_{p,1} - E_{p,2} = 0.130$  V and  $I_{p,2}/\vec{I}_{E=E_{p,2}} = 2.2$ , which corresponds to the ratio  $\kappa_2/\kappa_1 = 4.7$  [31]. Considering some other data published for methanol [22-23] and ethanol [32], an average ratio  $\kappa_2/\kappa_1 = 2.5 \pm 0.5$  was calculated. These show that the proposed indicator can be used for the estimation of an increased activity of the catalyst after the reactivation in the electro-oxidation of methanol [29-30], ethanol [35], glycerol [38] and formic acid [39].

## Conclusions

The proposed model takes in consideration the edge effects on a partially blocked electrode and the change of concentration profiles during the complete blockade. So, it is proper to describe an irreversible electro-oxidation that is complicated by the potential dependent inactivation and reactivation of the electrode surface. The model predicts that the second anodic peak that appears in the reverse, cathodic

branch of cyclic voltammogram depends on the kinetics of the electrode reaction after the reactivation of the surface. A ratio between the second peak current and the current at the same potential in the anodic branch is proposed as an indicator of the difference in electrode kinetics, before and after the inactivation. This ratio is independent of the scan rate. If the kinetic parameter does not change, the ratio is equal to 0.77 and does not depend on the difference between the potentials of the first and second peaks. Generally, this ratio is a linear function of the logarithm of the ratio between rate constants on the initial and the reactivated electrode surface. The model is formal and does not consider the actual mechanism of the inhibition of the electrode reaction.

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